See also problem

Problemè 1

In Lab 4, We used a PD compensator to control our ball and beam apparatus. The transfer function of our PD compensator was as follows:

$$G_C(s) = K_D s + K_P$$

However, we did not use the compensator in this form. The transfer function we used in lab was as follows:

$$G_C(s) = K_C(s+z)$$

② Question

Solve for K_C and z in terms of K_P and K_D .

Given

$$G_C(s) = K_C(s+z)
onumber \ G_C(s) = K_D s + K_P$$

Or it can be written as:

$$(K_C - K_D)s + K_C z - K_P = 0$$

To solve for the characteristic equation, we can set the coefficients of s and the constant term to zero:

$$K_C - K_D = 0$$

 $K_C z - K_P = 0$

Thus, we can solve for K_C and z as follows:

$$egin{aligned} K_C &= K_D \ z &= rac{K_P}{K_C} = rac{K_P}{K_D} \end{aligned}$$

Problemè 2

Given that the transfer function of our Ball and Beam plant used in the previous lab is as follows:

$$G(s)=rac{0.419}{s^2}$$

And given that the controller is applied to the plant in cascade configuration, find:

2.a

Static error constant for position (position constant)

This is a Type-2 system, thus position constant $K_p=\infty$

② 2.b

Static error constant for velocity (velocity constant)

Velocity constant $K_v = \lim_{s o 0} sG(s) = \lim_{s o 0} rac{0.419s}{s^2} = \infty$

② 2.c

Static error constant for acceleration (acceleration constant)

Acceleration constant $K_a = \lim_{s o 0} s^2 G(s) = \lim_{s o 0} rac{0.419 s^2}{s^2} = 0.419$

② 2.d

Steady-state error for a step input u(t)

For a step input $R(s) = \frac{1}{s}$, the steady-state error is given by:

$$e_{ss}=\lim_{s
ightarrow 0}rac{R(s)}{1+K_pG(s)}=\lim_{s
ightarrow 0}rac{1/s}{1+\infty}=0$$

② 2.e

Steady-state error for a ramp input tu(t)

For a ramp input $R(s) = \frac{1}{s^2}$, the steady-state error is given by:

$$e_{ss} = \lim_{s o 0} rac{sR(s)}{1+K_v G(s)} = \lim_{s o 0} rac{s/s^2}{1+0.419} = rac{1}{0.419} pprox 2.39$$

② 2.f

Steady-state error for a parabolic input $t^2u(t)$

For a parabolic input $R(s) = \frac{1}{s^3}$, the steady-state error is given by:

$$e_{ss} = \lim_{s o 0} rac{s^2 R(s)}{1 + K_a G(s)} = \lim_{s o 0} rac{s^2/s^3}{1 + 0.419} = rac{1}{0.419} pprox 2.39$$

Problemè 3

We will be augmenting our controller to include an integrator. The transfer function of our new PID compensator will be as follows;

$$G_C(s) = K_D s + K_P + rac{K_I}{s}$$

Given that the transfer function for our plant has not changed, and given that this controller is also applied to the plant in cascade configuration.

The closed-loop transfer function is

$$\frac{Y(s)}{R(s)} = \frac{G(s)G_C(s)}{1+G(s)G_C(s)} = \frac{\frac{0.419}{s^2} * (K_Ds + K_P + \frac{K_I}{s})}{1 + \frac{0.419}{s^2} * (K_Ds + K_P + \frac{K_I}{s})} = \frac{0.419 * (K_Ds + K_P + \frac{K_I}{s})}{s^2 + 0.419 * (K_Ds + K_P + \frac{K_I}{s})}$$

(?) 3.a

Static error constant for position (position constant)

$$K_P = \lim_{s o 0} G_C(s) G(s) = \lim_{s o 0} rac{0.419}{s^2} (K_D s + K_P + rac{K_I}{s}) = \infty$$

② 3.b

Static error constant for velocity (velocity constant)

$$K_V = \lim_{s o 0} sG_C(s)G(s) = \lim_{s o 0} s rac{0.419}{s^2} (K_D s + K_P + rac{K_I}{s}) = 0.419 K_D + rac{0.419 K_P}{s} + rac{0.419 K_I}{s^2} = 0.419 K_D$$

② 3.c

Static error constant for acceleration (acceleration constant)

$$K_A = \lim_{s o 0} s^2 G_C(s) G(s) = \lim_{s o 0} s^2 rac{0.419}{s^2} (K_D s + K_P + rac{K_I}{s}) = 0.419 K_P$$

② 3.d

Steady-state error for a step input u(t)

For a step input $R(s) = \frac{1}{s}$, the steady-state error is given by:

$$e_{ss} = \lim_{s o 0} rac{sR(s)}{1 - rac{C(s)}{R(s)}} = \lim_{s o 0} s rac{1/s}{1 - rac{C(s)}{R(s)}} = rac{1}{1 + K_P} = 0$$

② 3.e

Steady-state error for a ramp input tu(t)

For a ramp input $R(s) = \frac{1}{s^2}$, the steady-state error is given by:

$$e_{ss} = \lim_{s o 0} rac{s^2 R(s)}{1 - rac{C(s)}{R(s)}} = \lim_{s o 0} rac{s^2/s^2}{1 - rac{C(s)}{R(s)}} = rac{1}{K_V} = rac{1}{0.419 K_I}$$

② 3.f

Steady-state error for a parabolic input $t^2u(t)$

For a parabolic input $R(s) = \frac{1}{s^3}$, the steady-state error is given by:

$$e_{ss} = \lim_{s o 0} rac{s^3 R(s)}{1 - rac{C(s)}{R(s)}} = \lim_{s o 0} rac{s^3/s^3}{1 - rac{C(s)}{R(s)}} = rac{1}{K_A} = rac{1}{0.419 K_P}$$

Problemè 4

Ideally you want your controller design to reject a step disturbance input at D(s). This means that in the steady state for $D(s) = \frac{1}{s}$, the output Y(s) is unchanged.

? **4.**a

Ignoring the input R(s), what is the transfer function $\frac{E(s)}{D(s)}$ in terms of $G_1(s)$ and $G_2(s)$?

To find the transfer function $\frac{E(s)}{D(s)}$, then the transfer function $\frac{E(s)}{D(s)}$ is given by:

$$rac{E(s)}{D(s)} = rac{G_1(s)G_2(s)}{1+G_1(s)G_2(s)}$$

? 4.b

For $G_1(s) = K_C(s+z)$ and $G_2(s) = \frac{0.419}{s^2}$ what is the steady state error resulting from step inputs $R(s) = \frac{A}{s}$ and $D(s) = \frac{B}{s}$

The steady-state error to step input $R(s) = \frac{A}{s}$ is given by:

$$e_{ss}(R) = \lim_{s
ightarrow 0} rac{A}{s}(rac{1}{1+L(s)})$$

with $L(s) = G_1(s)G_2(s) = rac{0.419K_C(s+z)}{s^2}$

$$e_{ss}(R) = \lim_{s o 0} rac{A}{s} (rac{1}{1 + rac{0.419K_C(s+z)}{s^2}}) = rac{A}{0.419K_C}$$

The steady-state error to step input $D(s) = \frac{B}{s}$ is given by: $e_{ss}(D) = \frac{B}{0.419K_C}$

Thus, the total steady-state error is $e_{ss} = e_{ss}(R) + e_{ss}(D) = rac{A+B}{0.419K_C}$

? 4.c

For $G_1(s) = K_D s + K_P + \frac{K_I}{s}$ and $G_2(s) = \frac{0.419}{s^2}$ what is the steady state error resulting from step inputs $R(s) = \frac{A}{s}$ and $D(s) = \frac{B}{s}$

$$L(s) = G_1(s)G_2(s) = rac{0.419(K_Ds+K_P+rac{K_I}{s})}{s^2} = rac{0.419K_Ds^2+0.419K_Ps+0.419K_I}{s^3}$$

The steady-state error to step input $R(s) = \frac{A}{s}$ is zero:

$$e_{ss}(R) = \lim_{s o 0} rac{A}{s} (rac{1}{1+L(s)}) = \lim_{s o 0} rac{A}{s} (rac{1}{1+rac{0.419K_Ds^2+0.419K_Ps+0.419K_I}{s^3}}) = 0$$